# Trajectory planning based on hand operation for the un-redundant arm of service robot 

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#### Abstract

Any unfamiliar motions of the arm for service robot will make people anxious and human-like arm motion may be a solution. A virtual prototype of service robot with dual 6DOF (Degree of Freedom) arms named FISR (Family Intelligent Service Robot) has been developed. The application of service robot is not only performing human-like arm motion but also focusing on the hand operation such as grasping an object. So based on hand operation a formulation of elbow elevation angle is constructed to plan human-like arm motion for FISR. Furthermore a strategy about how to grasp a convex object is proposed.


Key-Words: - Elbow elevation angle, human-like trajectory, hand operation, un-redundant arm, service robot

## 1 Introduction

The research on the effect of manipulator motion on human psychology in last several years shows that people who staying near a manipulator will feel nervous if manipulator motions are not familiar to them ${ }^{[1]-[10]}$. It is a necessary for service robot using human-like arm motion when working with human. ${ }^{[11]-[20]-}$
T.Asfour et al. ${ }^{[21]}$ proposed an approach to generate human-like arm motion using mathematical representation with 7DOF arm. Seungsu Kim et al. ${ }^{[22]}$ developed an approach of using Response Surface Methodology to calculate the elbow elevation angle from human motion for a robot with 6DOF per-arm. Nancy S.Pollard et al. ${ }^{[23]}$ realize a humanoid robot that
consist of only an upper body adapting pre-recorded human motion and trajectory. Nakaoka et al. ${ }^{[24]}$ explored a procedure to make a humanoid robot(HRP-1S) imitate a Japanese folk dance captured by a motion capture system. J.F.Soechting et al. ${ }^{[25]}$ concluded that the Donder' law is not hold for pointing movements of the human arm which means the elbow elevation angle is not determined by the wrist location only.
A 6DOF manipulator is popular in industry, so it will be widely used as the arm of service robot. It is not applicable for only realizing the arm motion human-like, but ignoring its hand operational functions. It hasn't been studied yet about how to synthesize both of these two requirements in a 6DOF arm of service robot. In order to study it a mobile service robot with two

6DOF arms named FISR has been developing in our lab. Its DOF configuration is based on the angle defining the posture of the human arm. ${ }^{[26]}$ In this paper a formulation of elbow elevation angle is constructed for FISR based on the inverse kinematics equations and the qualitative relationship between the palm direction and the elbow elevation angle. A strategy on how to determine an arm motion to grasp a convex object is proposed. A simulation of FISR using its right hand to grasp a box with human-like arm motion is presented in the end.

## 2 Derivation of Human-like Arm

## trajectory

### 2.1 Angles defining the posture of human arm

Based on the results in ${ }^{[26]}$, a sketch map of human right arm is depicted in Figure 1. We define $v$ to be the angle between the perpendicular P to the plane of the arm and the horizontal plane. An equation can be derived: $\sin v=\sin \alpha \sin \zeta$, the parameter
$v$ is elbow elevation angle for a given hand location and the result of that elbow angle
$\phi$ depends only on the hand location.


Fig. 1 Angles defining human arm posture

### 2.2 Forward kinematics of FISR

Each arm of FISR has 6DOF revolute joints with a gripper and the body uses 3 Omni-wheels. The Denavit-Hartenberg (D-H) convention and methodology are used in this section to derive its kinematics. The coordinate frame assignment and the D-H parameters are depicted in Figure 2 and listed in Table 1 respectively, where $\left(x_{0}, y_{0}, z_{0}\right)$ represents the local coordinate frame at the body, $\left(x_{1}, y_{1}, z_{1}\right)$ to $\left(x_{6}, y_{6}, z_{6}\right)$ represent the local coordinate frames at the six joints respectively, $\left(x_{h}, y_{h}, z_{h}\right)$ is local coordinate frames at the hand, the $\alpha, \gamma, \theta$ are the rotation angles about $x, y$, and $z$ respectively. The description of the coordinate transformation from frame $i$ to $i+1$ is given by:
${ }^{i} T_{i+1}=\operatorname{Rot}\left(y_{i}, \gamma_{i}\right) \operatorname{Trans}\left(y_{i}, d_{i}\right)$
$\operatorname{Rot}\left(x_{i+1}, \alpha_{i+1}\right) \operatorname{Trans}\left(x_{i+1}, a_{i+1}\right) \operatorname{Rot}\left(z_{i+1}\right.$,
$\theta_{i+1}$ ), $i=0,1 \ldots n \quad s$ and $c$ mean mathematical symbols $\sin$ and cos in the formulations respectively.


Fig. 2 DOF configuration of FISR

| Table 1 D-H parameters for FISR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Link | $\theta$ | $d(\mathrm{~mm})$ | $a(\mathrm{~mm})$ | $\gamma$ | $\alpha$ |
| 1 | $\theta_{1}$ | 0 | $a_{1}=$ <br> 300 | $0^{\circ}$ | $0^{\circ}$ |
| 2 | $\theta_{2}$ | 0 | 0 | $0^{\circ}$ | $-90^{\circ}$ |
| 3 | $\theta_{3}$ | $d_{2}=$ <br> 268 | 0 | $-90^{\circ}$ | $-90^{\circ}$ |
| 4 | $\theta_{4}$ | 0 | 0 | $0^{\circ}$ | $90^{\circ}$ |
| 5 | $\theta_{5}$ | $d_{4}=$ <br> 158 | 0 | $-90^{\circ}$ | $-90^{\circ}$ |
| 6 | $\theta_{6}$ | 0 | 0 | $0^{\circ}$ | $-90^{\circ}$ |

According to ${ }^{[26]}$ and ${ }^{[27]}$ we can define the range of the parameters $\theta_{1} \sim \theta_{6}$ represented in Table. 2 which are in the range of rotation angle for human arm joints. It also can be generated an equation $\sin v=-\sin \theta_{2} \cos \theta_{3}$ based on the forward kinematics of FISR.

| Table 2 Joints angle range |  |  |  |
| :---: | :---: | :---: | :---: |
| Link/Joints | $\theta$ | Range |  |
| $1 / 0-1$ | $\theta_{1}$ | $-50^{\circ} \sim 0^{\circ}$ | $0^{\circ} \sim 130^{\circ}$ |
| $2 / 1-2$ | $\theta_{2}$ | $-1^{\circ} \sim-90^{\circ}$ | $-1^{\circ} \sim-120^{\circ}$ |
| $3 / 2-3$ | $\theta_{3}$ | $-90^{\circ} \sim 90^{\circ}$ |  |
| $4 / 3-4$ | $\theta_{4}$ | $0^{\circ} \sim-150^{\circ}$ |  |
| $5 / 4-5$ | $\theta_{5}$ | $-80^{\circ} \sim 80^{\circ}$ |  |
| $6 / 5-6$ | $\theta_{6}$ | $-70^{\circ} \sim 80^{\circ}$ |  |

### 2.3 Human-like elbow elevation angle

In order to make the arm motion human-like based on hand operation, it is necessary to use 4 joints on the shoulder and elbow to control arm posture which includes the elbow elevation angle.

$$
\begin{aligned}
& {\left[\begin{array}{cc}
R_{6} & P_{6} \\
0 & 1
\end{array}\right]=\left[\begin{array}{cccc}
n_{6 x} & o_{6 x} & a_{6 x} & p_{6 x} \\
n_{6 y} & o_{6 y} & a_{6 y} & p_{6 y} \\
n_{6 x} & o_{6 z} & a_{6 z} & p_{6 z} \\
0 & 0 & 0 & 1
\end{array}\right] \text { and }} \\
& {\left[\begin{array}{cc}
R_{h} & P_{h} \\
0 & 1
\end{array}\right]=\left[\begin{array}{cccc}
n_{h x} & o_{h x} & a_{h x} & p_{h x} \\
n_{h y} & o_{h y} & a_{h y} & p_{h y} \\
n_{h z} & o_{h z} & a_{h z} & p_{h z} \\
0 & 0 & 0 & 1
\end{array}\right]}
\end{aligned}
$$

represent the posture of wrist and hand at the coordinate frame of $\left(x_{0}, y_{0}, z_{0}\right)$ respectively. The following equation can be derived: $\left[\begin{array}{cc}R_{6} & P_{6} \\ 0 & 1\end{array}\right]=\left[\begin{array}{cc}R_{h} & P_{h} \\ 0 & 1\end{array}\right]\left({ }^{6} T_{h}\right)^{-1}$. Let's define $f=\sin v=-s \theta_{2} c \theta_{3}$. So there is an equation. The following formulations can be generated:
$p_{6 x}$
$=300-158\left(c \theta_{1} c \theta_{2} s \theta_{3}-s \theta_{1} c \theta_{3}\right) s \theta_{4}$
$-158 c \theta_{1} s \theta_{2} c \theta_{4}-268 c \theta_{1} s \theta_{2}$
$p_{6 y}$
$=-158\left(s \theta_{1} c \theta_{2} s \theta_{3}+c \theta_{1} c \theta_{3}\right) s \theta_{4}$
$-158 s \theta_{1} s \theta_{2} c \theta_{4}-268 s \theta_{1} s \theta_{2}$
$p_{6 z}$
$=158 s \theta_{2} s \theta_{3} s \theta_{4}-158 c \theta_{2} c \theta_{4}-268 c \theta_{2}$
$f=-s \theta_{2} c \theta_{3}$
According to the cosine theorem the formulation can be obtained:
$\left(p_{6 x}-300\right)^{2}+p^{2}{ }_{6 y}+p^{2}{ }_{6 z}$
$=158^{2}+268^{2}-2 * 158 * 268 c\left(\pi+\theta_{4}\right)$

The solution for $\theta_{4}$ is as follows.
$\theta_{4}=\arccos \frac{D}{-2 * 158 * 268}-\pi$
D
$=\left(p_{6 x}-300\right)^{2}+p^{2}{ }_{6 y}+p^{2}{ }_{6 z}-158^{2}-268^{2}$

If $s \theta_{4}=0$, the solution for $\theta_{2}$ can be resulted from (3)
$\theta_{2}=-\arccos \left(\frac{p_{6 z}}{-426}\right)$
If $\theta_{4} \neq 0$, the following formulation can be derived from (3) and (4):
$0=\left(\left(158 c \theta_{4}+268\right)^{2}+\left(158 s \theta_{4}\right)^{2}\right) c \theta_{2}{ }^{2}$
$+2 p_{6 z}\left(158 c \theta_{4}+268\right) c \theta_{2}+\left(158 s \theta_{4}\right)^{2} f^{2}$
$+p_{6 z}{ }^{2}-\left(158 s \theta_{4}\right)^{2}$

In order to ensure the formulation (8) has solutions, the following equation should be satisfied.
$\Delta=$
$-4 *\left(158 s \theta_{4}\right)^{2} \cdot\left(\left(268^{2}+2 * 268 * 158 c \theta_{4}\right.\right.$
$\left.\left.+158^{2}\right)\left(f^{2}-1\right)+p_{6 z}{ }^{2}\right)$

There is relationship between the elbow elevation angle and the palm direction. ${ }^{[27]}$ ${ }^{[28]}$ It can be intuitively noticed that when the palm direction is upward vertically the elbow elevation angle is usually close to zero, but it will become larger gradually during the palm direction transits from the upward vertically to the downward vertically. So a factor $1-e^{n_{62}-1}$ is used here to indicate the relationship between the palm direction and the elbow elevation angle. Although it is difficult to represent the relationship of these two angles precisely, since there are many personalities
in arm motion, its qualitative representation is enough to make the arm motion of FISR human-like. The equation of (9) will be satisfied if the following formulation exists.

$$
f=\sqrt{(1-d)\left(1-e^{n_{\delta_{2}-1}-1}\right)}
$$

$$
\begin{equation*}
d=\frac{p_{6 z}{ }^{2}}{268^{2}+2 * 268 * 158 c \theta_{4}+158^{2}} \tag{10}
\end{equation*}
$$

Then we can get another solution for $\theta_{2}$, and solutions for other joints in the arm.

### 2.4 A strategy for grasping a convex object

Grasping an object is an important function for service robot. If the center of coordinate frame $\left(x_{h}, y_{h}, z_{h}\right)$ is in an object, it can be believed that the object can be grasped. In order to plan a motion of grasping an object, an initial posture of $\left(x_{h}, y_{h}, z_{h}\right)$ for the hand to grasp the object should be chosen. Then the joints angle can be derived from the inverse kinematics of the arm. Based on the forward kinematics, a hand posture can be derived then. If it doesn't equal the initial posture, there must be a rotation on the axes of $x_{h}$ in the initial posture and the angle can be represented as $\alpha$. Let's rotate the coordinate frame of initial posture on its axes of $x_{h}$ for $\frac{\alpha}{2}$, and the result can be used as the initial posture for the next iterative calculation. The iterative computing will stop until the rotation $\alpha$ is in the range of the threshold or there are too many iterative times. The initial value of $\alpha$ is zero, and its threshold is 0.2 in this paper. The posture of $\left(x_{6}, y_{6}, z_{6}\right)$ can be

$$
\text { determined } \quad \text { by } \quad\left[\begin{array}{cc}
R_{6} & P_{6} \\
0 & 1
\end{array}\right]
$$

$$
=\left[\begin{array}{cc}
R_{h} & P_{h} \\
0 & 1
\end{array}\right] \operatorname{Rot}\left(x_{h}, \frac{\alpha}{2}\right) \operatorname{Trans}\left(y_{h}, 100\right) .
$$

After the posture of the hand to grasp an object is determined, the trajectory of its transiting from the current location to the final location can be planed. The distance and the posture of the wrist from the current location to the final location are denoted as $D_{i}$ and $\Delta R_{i}$, let's suppose $\frac{\Delta R_{i}}{\Delta R_{0}}=\frac{D_{i}}{D_{0}}$.

## 3 Simulation and Discussions

A simulation of grasping a box is implemented with the right hand to illustrate how to pick up an object with human-like motion for the un-redundant arm of FISR. There is a box 60 mm long and wide, 110 mm high mounted upon a horizontal table. Suppose the center of initial posture of $\left(\begin{array}{lll}x_{h} & y_{h} & z_{h}\end{array}\right)$ is at the center of the box and the $x_{h}$ perpendicular to a plane of the box. Its initial posture of the hand is $\left[\begin{array}{cccc}-0.707 & 0.707 & 0 & 30.0 \\ -0.707 & -0.707 & 0 & 300.0 \\ 0 & 0 & 1 & -250.0 \\ 0 & 0 & 0 & 1\end{array}\right]$
the coordinate frame $\left(x_{0}, y_{0}, z_{0}\right)$. So the initial wrist posture of $\quad\left(\begin{array}{lll}x_{6} & y_{6} & z_{6}\end{array}\right) \quad$ is

$$
\left[\begin{array}{cccc}
-0.707 & 0.707 & 0 & 100.7 \\
-0.707 & -0.707 & 0 & 229.3 \\
0 & 0 & 1 & -250.0 \\
0 & 0 & 0 & 1
\end{array}\right]
$$

The strategy on how to determine a hand posture to pick up a box is presented. The desired posture for ( $\left.\begin{array}{lll}x_{h} & y_{h} & z_{h}\end{array}\right)$ in the final has rotated $13.1^{\circ}$ clockwise on the axes $x_{h}$ relative to the initial posture.

Suppose the current posture of the arm for FISR is as depicted in Figure 2 whose joints angle are $\theta_{1}=0^{\circ}, \theta_{2}=-1^{\circ}, \theta_{3}=0^{\circ}, \theta_{4}=0^{\circ}$,
$\theta_{5}=0^{\circ}, \theta_{6}=0^{\circ}$, and the trajectory of wrist to transit from the current location to the final location is a straight line. The solutions of the parameters in the motion for grasping the box are presented in Figure 3 and listed in Table. 3.
The first drawing in Figure 3 is the solutions of six joints in the motion of grasping the box. The second drawing is the value of elbow elevation angle in the motion. It is obviously that when the hand is raised more quickly than the elbow, the elbow elevation angle is becoming larger for the perpendicular to the plane constructed with points shoulder, wrist and elbow rotated from vertical direction to horizontal direction. The transition of elbow elevation angle is similar to human arm motion in this operation. In the last drawing '*’, 'o' and ‘• ' represent the location of elbow, wrist and hand at the coordinate frame of $\left(x_{0}, y_{0}, z_{0}\right)$ respectively. In simulations the manipulator transformed from the posture of hanging vertically to almost rising horizontal. The wrist moved backward first
and then forward when the robot bent its arm and put its hand on the table. The results demonstrate the strategy to plan a
human-like motion with the un-redundant arm to grasp a convex object is effective.

| Table 3 The parameters in iterative process |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Times | $\left(x_{6}, y_{6}, z_{6}\right)$ | $\alpha$ | $\alpha / 2$ | $\theta_{1}$ | $\theta_{2}$ | $\theta_{3}$ | $\theta_{4}$ | $\theta_{5}$ | $\theta_{6}$ | $f$ |
| 1 | $(100.7,229.3,-250)$ | 19.8 | 9.9 | 110.6 | -41.9 | 23.1 | -46.8 | 47.2 | -19.5 | 0.614 |
| 2 | $(99.6,230.4,-232.8)$ | 4.7 | 2.35 | 108.4 | -43.0 | 22.0 | -53.3 | 46.2 | -22.6 | 0.632 |
| 3 | $(99.1,230.9,-228.8)$ | 1.2 | 0.6 | 108.1 | -43.3 | 21.9 | -54.5 | 46.1 | -23.1 | 0.637 |
| 4 | $(98.9,231.1,-227.8)$ | 0.4 | 0.2 | 108.0 | -43.4 | 21.9 | -54.7 | 46.0 | -23.2 | 0.638 |
| 5 | $(98.9,231.1,-227.4)$ | 0.1 | 0.05 | 108.0 | -43.5 | 21.9 | -54.8 | 46.0 | -23.3 | 0.638 |

Six Joints Angle in the Motion



Elbow/Wrist/Hand Positions


Fig. 3 Solutions of the parameters in motion

## 4 Conclusion

It is the first approach of planning human-like motion based on hand operation
for the un-redundant arm of FISR. A strategy on how to determine a posture of the hand to grasp a convex object and plan the human-like arm motion is proposed. Although a 6-DOF manipulator can be yielded an effective posture for grasping an object in Cartesian coordinate. But in order to grasp an object in real world will not using only one posture. So if a posture can grasp the object and it is human-like will be much better than a normal posture only satisfies the grasping function. The approach is one attempt for realizing this dream. The method can be applied in other service robot using 6DOF arm to realizing hand operation with human-like arm motion. Furthermore it can also be applied in the 7 -freedom manipulator which can grasp objects with many kinds of postures.

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## Appendix

The following formulations focus on the solutions of $\theta_{2}$ will always exist on equation (8).
According to the equation (9), the following formulations can be derived.
$\left(268^{2}+2 * 268 * 158 c \theta_{4}+158^{2}\right)\left(f^{2}-1\right)$
$+p_{22}{ }^{2} \leq 0$
$c \theta_{2}=\frac{F}{E}$
$F=-p_{2 z}\left(158 c \theta_{4}+268\right)$
$\pm 158\left|s \theta_{4}\right| \cdot \sqrt{-\left(E^{2}\left(f^{2}-1\right)+p_{2 z}{ }^{2}\right)}$
$E=268^{2}+2 * 268 * 158 c \theta_{4}+158^{2}$
$\frac{F}{E} \leq \frac{G}{E}$
$F=-p_{2 z}\left(158 c \theta_{4}+268\right) \pm 158\left|s \theta_{4}\right| \sqrt{E^{2}-p_{2 z}{ }^{2}}$
For $\theta_{4} \in[0, \pi]$ and $f \in[-1,1]$
$\frac{G}{E} \leq \frac{H}{E}$
$H=-\left(158 c \theta_{4}+268\right) s \alpha-158 s \theta_{4} c \alpha$
For $p_{2 \tau} \geq 0$ and $\alpha \in\lfloor 0, \pi / 2\rfloor$
$c \alpha=\frac{\sqrt{E^{2}-p_{2 z}{ }^{2}}}{E}$
$s \alpha=\frac{p_{2 z}}{E}$
$I=E^{2}-H^{2}$
$I \geq J$
$J$
$=2 \cdot 268 \cdot 158 c \theta_{4}$
$+2 \cdot 268 \cdot 158|c \alpha| \cdot\left|c\left(\theta_{4}+\alpha\right)\right|$
$-2 \cdot 268 \cdot 158 s \alpha s\left(\theta_{4}+\alpha\right)$
If $c\left(\theta_{4}+\alpha\right)>0$, so $\theta_{4}+\alpha \in(0, \pi / 2)$,
J
$=2 * 268 * 158 c \theta_{4}+2 * 158 * 268 c\left(\theta_{4}+2 \alpha\right)$
$=2 * 268 * 158\left(c \theta_{4}+c\left(\theta_{4}+2 \alpha\right)\right)$
Because $\theta_{4} \in[0, \pi] \quad, \quad \alpha \in\lfloor 0, \pi / 2\rfloor$,
$\theta_{4}+\alpha \in(0, \pi / 2)$, so $\theta_{4} \in\lfloor 0, \pi / 2\rfloor$.
If $\theta_{4}+2 \alpha \in\lfloor 0, \pi / 2\rfloor$, we can derived that
$\theta_{4} \in\lfloor 0, \pi / 2\rfloor$ and $\theta_{4} \leq \theta_{4}+2 \alpha$, so
$J \geq 0$.
If $\theta_{4}+2 \alpha \in\lfloor\pi / 2, \pi\rfloor$, we can derived
that

$$
\pi-\left(\theta_{4}+2 \alpha\right) \in\lfloor 0, \pi / 2\rfloor
$$

$-c\left(\theta_{4}+2 \alpha\right)=c\left(\pi-\left(\theta_{4}+2 \alpha\right)\right) \geq 0$, and
because

$$
\pi-\left(2 \theta_{4}+2 \alpha\right) \geq 0
$$

$\pi-\left(\theta_{4}+2 \alpha\right) \geq \theta_{4}, \theta_{4} \in\lfloor 0, \pi / 2\rfloor$.
So $c \theta_{4} \geq\left|c\left(\theta_{4}+2 \alpha\right)\right|$, so $J \geq 0$
So the solutions are in the range of $[-1,1]$.

## Reference

[1] Dana Kulíc and Elizabeth Croft , "Physiological and subjective responses to articulated robot motion" , Robotica (2007) volume 25, pp. 13-27.
[2] Y.Matsumoto, J.Heinzmann, A.Zelinsky, "The Essential Components of Human-Friendly Robot Systems", Proceedings of the International Conference on Field and Service Robotics, pp.43-51, Pittsburgh, USA,August 29-31, 1999.
[3] Dana KuliC Elizabeth Croft ,"Safe Planning for Human-Robot Interaction", ProCMdlngL of the 2004 IEEE Inmrnational Conhnnce on Robtics 6 Automation New Orleans. LA \&rll2004.
[4] Hong Liu, Xuezhi Deng and Hongbin Zha, "A planning method for safe interaction between human arms and robot manipulators", Intelligent Robots and Systems, 2-6 Aug, 2005. (IROS 2005) ,Page(s):2724-2730.
[5] Kulic, D., Croft, E., "Anxiety detection during human-robot interaction", Intelligent Robots and Systems, 2-6 Aug, 2005,Page(s):616 - 621.
[6] Shibata, S., Ohba, K., Inooka, N.,"Emotional evaluation of human arm motion models", Robot and Human Communication. Proceedings., 2nd IEEE International Workshop on 3-5 Nov. 1993 Page(s):346-351
[7] Kulic, D., Croft, E., "Estimating Robot

Induced Affective State using Hidden Markov Models", Robot and Human Interactive Communication. ROMAN 2006. The 15th IEEE International Symposium on Sept. 2006 Page(s):257 262.
[8] Seungsu Kim, Chang Hwan Kim, ChangHwan Kim, "Human-like Arm Motion Generation for Humanoid Robots Using Motion Capture Database", Intelligent Robots and Systems, 2006 IEEE/RSJ International Conference on Oct. 2006 Page(s):3486-3491.
[9] Traver, V.J., del Pobil, A.P., Perez-Francisco, M, "Making service robots human-safe", Intelligent Robots and Systems, 2000. (IROS 2000). Proceedings. 2000 IEEE/RSJ International Conference on Volume 1, 31 Oct.-5 Nov. 2000 Page(s):696-701 vol.1.
[10]Heinzmann, J., Zelinsky, A, "The safe control of human-friendly robots", Intelligent Robots and Systems, 1999. IROS '99. Proceedings. 1999 IEEE/RSJ International Conference on Volume 2, 17-21 Oct. 1999 Page(s):1020 - 1025 vol.2.
[11]Auke Jan Ijspeert \& Jun Nakanishi \& Stefan Schaal, "Movement Imitation with Nonlinear Dynamical Systems in Humanoid Robots", Proceedings of the IEEE International Conference on Robotics and Automation, 2002
[12]Sylvain Calinon, Florent Guenter and Aude Billard, "Goal-Directed Imitation in a Humanoid Robot", Proceedings of the 2005 IEEE International Conference on Robotics and Automation Barcelona, Spain, April 2005.
[13]Sylvain Calinon \& Aude Billard,"Stochastic gesture production and recognition model for a humanoid robot", Proceedings of the 2004 IEEE/RSJ

International Conference on Intelligent Robots and Systems, Septemeber 28-October 2, 2004, Sendai, Japan.
[14]L. Rabiner,"A tutorial on hidden markov models and selected applications in speech recognition", Proceedings of the IEEE, vol.77:2, pp. 257-285, February 1989
[15]Aude G. Billard, Sylvain Calinon, Florent Guenter, "Discriminative and Adaptive Imitation in Uni-Manual and Bi-Manual Tasks", Robotics \& Autonomous Systems Journal, Dec. 2005.
[16]Tomomasa SATO, Yuichiro GENDA, Hideyuki KUBOTERA, Taketoshi MORI, Tatsuya HARADA, "Robot Imitation of Human Motion based on Qualitative Description from Multiple Measurement of Human and Environmental Data", Proceedings of the 2003 IEEE/RSJ International Conference on Intelligent Robots and Systems, Las Vegas, Nevada, October 2003.
[17]Tetsunari Inamura, Hiroaki Tanie, Yoshihiko Nakamura, "Keyframe Compression and Decompression for Time Series Data based on the Contimuous Hidden Markov Model", Proceedings of the 2003 IEEE/RSJ International Conference on Intelligent Robots and Systems, Las Vegas, Nevada, October 2003.
[18]Aaron P.shon, Keith Grochow, Rajesh P.N. Rao, "Robotic Imitation from Human Motion Capture using Gaussian Processes", Proceedings of 2005 5th IEEE-RAS International Conference on Humanoid Robots, 2005.
[19]Stefan Schaal, Auke Ijspeert and Aude Billard, "Computational Approaches to Motor Learning by Imitation", Philosophical Trasaction of the Royal Society of London: Series B, Biological Sciences 358:537-547. 2003.
[20]Aude Billard, Yann Epars, Sylvain Calinon, Stefan Schaal, Gordon Cheng, "Discovering optimal imitation strategies", Robotics and Autonomous Systems 47,69-77, 2004.
[21]T.Asfour, R.Dillmann, "Human-like Motion of a Humanoid Robot Arm Based on a Closed-Form Solution of the Inverse Kinematics Problem", Proceedings of the 2003 IEEE/RSJ Intl. Conference on Intelligent Robots and Systems, October.2003, vol. 2, pp. 1407-1412.
[22]Seungsu Kim, ChangHwan Kim and Jong Hyeon Park, "Human-like Arm Motion Generation for Humanoid Robots Using Motion Capture Database", Proceedings of the 2006 IEEE/RSJ International Conference on Intelligent Robots and Systems, Oct.9-15, 2006, pp.3486-3491.
[23]N. S. Pollard, J. K. Hodgins, Marcia J. Riley, and Christopher G. Atkeson, "Adapting human motion for the control of a humanoid robot," Proc. of IEEE Int. Conf. on Robotics and Automation, 2002, vol. 2, pp. 1390-1397.
[24]S. Nakaoka, A. Nakazawa, K. Yokoi, H. Hirukawa, and K. Ikeuchi, "Generating whole body motions for a biped humanoid robot from captured human dances," Proc. of Int. Conf. on Robotics and Automation, 2003, pp. 3905-3910.
[25]J.F.Soechting, Christopher A.Buneo, Uta Herrmann and Martha Flanders, "Moving Effortlessly in Three Dimensions: Does Donders' Law Apply to Arm Movement?", in the Journal of Neuroscience, pp:6271-6280, September 1995
[26]Somadeepti N.Chengalur et al., "KODAK'S Ergonomic Design for People at Work", Second Edition, John Wiley\&Sons, Inc., 2004.
[27]ChangHwan Kim, Seungsu Kim et al., "Regenerationg Human-like Arm Motions of Humanoid Robots for a Movable

Object", SICE Annual Conference 2007, pp.1081-1086, Kagawa University, Japan, Sept.17-20,2007.
[28]Derek G. Kamper, W. Zev Rymer, "Effects of geometric joint constraints on the selection of final arm posture during reaching: a simulation study", Exp.Brain Res. 1999 vol.126,pp134-38

